COMMUNICATION SYSTEM IDENTIFICATION THROUGH ADAPTIVE MODELING OF THE COMMUNICATION CHANNEL

BRIG. GEN. DR. NABIL M. ELNADY*    ENG. EMMANOEL S. HANNA**

ABSTRACT

In this paper, attempts are made to profile the radio propagation path linking an intercepted transmitter site to the signal collection facility. The main objective is to extract fingerprinting clues to identify the transmitter locality. Different methods of power spectrum estimation techniques are applied and compared w.r.t. their usefulness in identifying the multipath channel. A novel system is proposed to act as a transmitter locality identifier. The system is based on adaptive modeling of the faded channel. The system configuration is presented, the control software is developed and sample run-outs of the developed programs are presented and commented.

* The Chief of Chair of Electronic Warfare, the MTC, Cairo.
** Ph.D. Aspirant, the MTC, Cairo.
INTRODUCTION:

Multipath phenomenon [1] has always been very annoying when receiving electromagnetic waves transmitted from a distant locality. The multiplicity of propagation paths, especially when sky wave hops are involved, lead to the well-known fading effect. Fig.1 illustrates the different sky wave paths involved with a single hop communication channel.

![Diagram of Different sky wave propagation paths](image)

1. Lower effective boundary of the active ionospheric layer
2. Height of the maximum electron density
3. Upper effective boundary of the active ionospheric layer

--- Radiation paths with high and low angles of elevation, freq. much below MUF
--- Radiation paths with high and low angles of elevation, freq. only a little below MUF
--- Radiation path of the MUF
--- Radiation path of a frequency above the MUF

D. Skip distance at the MUF
θ. Angle of elevation of the radiation

In this paper we will utilize the multipath fading phenomenon to our advantage. We shall use this phenomenon to determine if a received signal is originating from the same area. The multipath affecting two independent signals is normally also independent. Thus the rate of fade in the two signal's spectrum will be different. This fact is very useful for determining if a complex signal is one signal or if it is actually the sum of two or more independent signals. The procedure for observing the multipath is to perform a frequency raster of the spectrum analyzer display. The equipment configuration for rastering the spectrum is shown in Fig.2. Two spectrum analyzers were used for this experiment, the HP5866S (Hewlett Packard model) and the SA5004/16 (Scientific Atlanta model). Control software was developed and records of the time history of the signal's spectrum were obtained (see Fig.3).
Multipath fading will create a null in the spectrum. The propagation path that a signal travels over changes with time. This change is usually very slowly varying, taking several seconds to minutes to observe. The effect on the signal's spectrum is to have the fading null change its position infrequency at different times. Thus a null at one instant of time will be observed to move across a signal's spectrum. Fig. 3 illustrates this phenomenon obtained experimentally in the laboratory using the above mentioned equipment configuration. It is shown in this figure that separate intercepted signals will have two distinctive null patterns representing their unique propagation paths.

DIFFERENT METHODOLOGIES FOR IDENTIFICATION OF THE PROPAGATION PATH:

In this paper we shall be concerned with the case of unmodulated carrier (with frequency \( f_c \)). The received signal for the case of discrete multipath is given by

\[
r(t) = \sum_{n} a_n(t) e^{-j2\pi f_c t} r_n(t)
\]

(1)

we expect that the delays \( r_n(t) \) associated with different signal paths to change at different rates and in a random manner. This implies that the received signal \( r(t) \) can be modeled as a random process. When there is a large number of paths, the central limit theorem can be applied. That is, \( r(t) \) can be modeled as a complex-valued Gaussian random process. This means that the time-variant impulse response \( c(r; t) \) is a complex-valued Gaussian random process the \( t \) variable. When the impulse response \( c(r; t) \) is modeled as a zero mean complex-valued Gaussian process, the envelope \( |c(r; t)| \) at any instant \( (t) \) is a Rayleigh-distributed \[2 \] and the channel is said to be a Rayleigh fading channel. In the case where there are fixed signal reflectors in the medium in addition to randomly moving scatterers, \( c(r; t) \) can no longer be modeled as having a zero mean. In this case, the envelope \( |c(r; t)| \) has a Rice distribution \[2 \] and the channel is said to be a Ricean fading channel. In our analysis we shall consider only the Rayleigh-distributed envelope statistics, a model often observed on HF and is widely accepted.
(a) - At 9 a.m.

Signal (1)
Signal (2)

Center freq. = 4 MHz
Transform Size = 2048
No. of Averages = 512
Freq. Range = 20 KHz

(b) - At 10 a.m.

Signal (1)
Signal (2)

Same Settings

(c) - At 11 a.m.

Signal (1)
Signal (2)

Same Settings

Fig. 3. The Time History of the Intercepted Signal Spectrum
The first methodology that we shall adopt in this paper is to characterize the fading multipath channel by suitable correlation and spectral density functions. Assume \( c(\tau; t) \) to be wide-sense stationary [4], then the autocorrelation function of \( c(\tau; t) \) is

\[
\phi_c(\tau_1, \tau_2; \Delta t) = \frac{1}{2} E \left[ c^*(\tau_1; t) c(\tau_2; t + \Delta t) \right]
\]

(2)

Most radio transmission media exhibit uncorrelated scattering; then the scattering at two different delays is uncorrelated. Thus (2) reduces to

\[
\frac{1}{2} E \left[ c^*(\tau_1; t) c(\tau_2; t + \Delta t) \right] = \phi_c(\tau_1; \Delta t) \delta(\tau_1 - \tau_2)
\]

(3)

At \( \Delta t = 0 \), \( \phi_c(\tau; 0) \) is the average power output of the channel as a function of the time delay \( \tau \). \( \phi_c(\tau) \) is called the Multipath Intensity Profile or the Delay Power Spectrum of the channel. In practice, the function \( \phi_c(\tau; \Delta t) \) is measured by transmitting a wide band signal (or equivalently very narrow pulses) and cross-correlating the received signal with a delayed version of itself. Fig.4a illustrates \( \phi_c(\tau) \). \( T_m \); (the range of values of \( \tau \) over which \( \phi_c(\tau) \) is essentially nonzero) is called the Multipath Spread of the Channel. An analogous characterization of the time-variant multipath channel can be performed in the frequency domain. \( \phi_c(\Delta f) \); the autocorrelation function in the frequency variable [4] is given by

\[
\phi_c(\Delta f) = \int_{-\infty}^{+\infty} \phi_c(\tau) e^{-j2\pi\Delta f \tau} d\tau
\]

(4)

This relationship is illustrated in Fig.4b.

![Fig.4. Multipath Intensity Profile](image)
(Δf) denotes the Coherence Bandwidth. Thus two frequencies separated by (Δf) are affected differently by the channel. If (Δf) < the bandwidth of the transmitted signal, the signal will be severely distorted by the channel. The channel is denoted in this case as a frequency selective channel. Due to the time variations of the channel Doppler shifts and broadening [3] occur. A function called the Scattering Function of the Channel can be characterized [4] and provides a measure of the average power output of the channel as a function of time delay τ and the Doppler frequency.

APPLYING ADAPTIVE TECHNIQUES

The second methodology presented here, which is the main contribution of the paper, is to apply adaptive techniques (which are emerging very rapidly in the field of digital signal processing). If the channel characteristics are known and are not varying with time and the signals received are well described and stationary, then the priori knowledge will enable the designer to determine the optimum signal processing method which can be used in the system all the time (e.g. fixed filters, Wiener filter, matched filters, etc.). The multipath faded channel cannot be handled in the same manner. Here we apply the principles of Linear Prediction to characterize the faded channel and to describe the channel via the LPC Parameters of the model (see Fig. 5).

![Fig. 5. Linear Predictive Coder for the Faded Channel](image)

The linear predictor adapts itself in a manner such that the residual signal power is minimized. It can be shown that if both the signal and the system are stationary, the parameters of the linear prediction filter are equal to the coefficients of the all-pole filter that is assumed to model the faded channel. A fast adaptation algorithm is needed such that the adaptive system may track the rapid changes in the faded channel during transmission. Intercepting remote broadcasting stations using an equipment configuration similar to that of Fig. 2, a control program (to control the HP5866S Spectrum Analyzer) was developed (see Appendix) to perform the following tasks:

1- Tuning the analyser to a maximum of seven frequencies, then measuring and displaying the time course of the instantaneous (and eventually the average) intensity of each signal. The results are displayed in Fig. 6.

2- In order to perform first hand comparison (in respect to the colocality of transmitting stations), the maximum amplitude excursion of the average intensity of each intercepted station is
Fig. 6. The Time Course of the Interceptions

Average Intensities
a- Instantaneous amplitude variations of an intercepted signal

b- Comparative Displays

Fig. 7. Qualitative Comparative Displays of Different Interceptions
Fig. 8. Instantaneous amplitude variations, LPC residual signal and the LPC Filter Coefficients for two distinctive signals.
then divided into three distinctive levels (characterized as $\pm$,$\&$,$\sim$). Fig.7 illustrates the obtained results which may guide in asserting quick recognition.

3-To model the intercepted channel as a 14-section LPC filter and to extract the coefficients of this filter. Fig.8 illustrates the averaged time course of an intercepted station, the residual signal out of the modeled filter and the parameters of the filter. Fig.9 illustrates the model for a suggested recognizer which is tasked to compare an intercepted channel to a channel model template. The template of the channel time course behaviour is chosen to be the LPC Parameters Array.

Thus intercepted channels are intercepted, their intensity-time dependence is monitored, the LPC-Model for each channel is constructed and its LPC-Parameters are evaluated. Then the LPC-Parameters are compared (using a suitable criterion, e.g. least squares) and the best fit yields the most probable site collocality.

We hope that the ideas presented here will prove futile for the mentioned tasking. Measurements performed have been promising. The analysis presented is applicable to other fields of interest (e.g. seismology).

CONCLUSION

The first methodology explained deals with characterizing the faded channel by the scattering function. This procedure has been adopted in many situations and involves a lot of mathematical computations. The suggested methodology of adaptive modeling applied to the faded channel promises fast results which can be encompassed in a database-oriented channel identification system.

REFERENCES


NOMENCLATURE

MUF: Max Usable Frequency.
$c(r,t)$: The time-variant impulse response of the equivalent low-pass channel.
Appendix
(Sample Flowcharts of the Developed Programs)

a - FLOW CHART FOR AMPLITUDE VS TIME

b - FLOW CHART FOR AMPLITUDE VS TIME
DIMENSION ARRAYS

INPUT START & STOP FREQUENCY

INPUT TIME POINTS ON SCREEN

INPUT FREQUENCY TO SURVEY INPUT

INPUT INTERVAL TIME BETWEEN MEASUREMENT

PREPARE SPECTRUM ANALYZER

START CYCLING & SCANNING

STORE DATA FOR EACH POINTS & FREQUENCY

TAKE AMPLITUDE FOR EVERY TIME

INDICATE MAX & MIN TO WAVEFORM FOR EACH FREQUENCY

DIVIDE THE DISTANCE BETWEEN MAX & MIN TO A BASELINE LEVEL

COMPARE THE LEVEL CROSSING FOR EACH FREQUENCY

PLOT THE RESULT OF COMPARING

END

START

DIMENSION ARRAY

INPUT FR, FS, CF, TD

PREPARE THE SPECTRUM ANALYZER

START CYCLING & SCANNING

TAKE AMPLITUDE FOR EVERY TIME (TD)

PLOT AND POINTS

STORE THE RESULT

EVALUATE THE LPC FILTER COEFFICIENT (ALL POLE MODES)

SELECT THE NUMBER OF FILTER SECTION OF LPC

CALCULATE THE AUTOCORRELATION COEFFICIENTS R(\#) = \sum_{k=0}^{N} x(k) x(k+\#)

EVALUATE THE 4TH ORDER OF INVERSE FILTER

EVALUATE THE TOTAL SQUARED ERROR \( \chi^2 \)

RETURN

C = FLOW CHART FOR AMPLITUDE COMPARISON

-------------------------------

D = FLOW CHART FOR LPC WAVEFORM
START

DIMENTION ARRAY

GENERATE THE IMPULSE TRAIN ACT AS A WHITE NOISE

READ DATA (LPC COEFFICIENT)

CALCULATE THE OUTPUT OF THE ALL-POLE SECTION

\[ D(Z) = E(Z) - \sum_{i} A_i Z^{-i} D(Z) \]

PLOT OUTPUT

END

e - FLOW CHART FOR SIMPLIFIED MODEL FOR WAVEFORM PRODUCTION